Phase II Monitoring of Generalized Linear Profiles Using Weighted Likelihood Ratio Charts

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Abstract

In recent years, effective profile monitoring for discrete response variables, such as binary, multinomial, ordinal or Poisson variables, has increasingly attracted interest of researchers in the area of statistical process control. Such quality characteristics are often modeled as special cases of generalized linear models. The objective of this paper is to try to provide a unified framework for Phase II monitoring of generalized linear profiles of which the explanatory variables can be fixed design or random arbitrary design. To this end, a new control chart is developed based on the weighted likelihood ratio test, and it can be readily extended to other generalized profiles or profiles with random predictors if the likelihood function can be obtained. Numerical results and illustrative example show that the proposed control chart has satisfactory in-control run length distribution and stands out at early detection.

Key words: Exponential Weighted Moving Average; Generalized Linear Model; Profile Monitoring; Statistical Process Control; Weighted Likelihood Ratio Test. *1991 MSC:* 62P30

1 Introduction

Statistical profile monitoring has increasingly attracted researchers' attention in the area of statistical process control. Early reviews of work in profile mon-

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itoring include Woodall et al. (2004) and Woodall (2007), and a recent comprehensive review Woodall and Montgomery (2014) recommend Noorossana et al. (2011) for a more up-to-date overview as the chapters in this book were written by some of the leading researchers in profile monitoring. For profile monitoring, one group of monitoring methods are interested in the case that the response variables are continuous (e.g., Li and Wang (2010); Zou et al. (2012); Huwang et al. (2014)). At the meantime, it is also quite common to deal with profile monitoring with discrete response variables. As far as we know, the pioneering work is Yeh et al. (2009). Some recent work, such as Amiri et al. (2011), Noorossana et al. (2013a), Noorossana et al. (2013b) and Soleymanian et al. (2013), focused on profile monitoring whose response variables are Poisson, ordinal, multinomial and binary variables, respectively.

In the case of discrete response variables, the quality characteristics are often modeled as special cases of generalized linear models (GLM). Amiri et al. (2015) and Shadman et al. (2015) provided a unified framework for Phase I control of generalized linear profiles. Besides the GLM, other types of models have also been used to represent profiles, such as simple linear regression (e.g., Zhang et al. (2009); Noorossana et al. (2010); Aly et al. (2015)), nonlinear regression (e.g., Chang and Yadama (2010); Paynabar et al. (2013)), multiple regression (e.g., Evvazian et al. (2011); Mahmoud et al. (2015)), nonparametric regression (e.g., Qiu et al. (2010); Chuang et al. (2013)), mixed models (e.g., Jensen and Birch (2009); Koosha and Amiri (2013)), and wavelet models (e.g., Chicken et al. (2009); Lee et al. (2012)). All of the afore-mentioned research, however, only consider the case in which the explanatory variables are fixed from profile to profile. Shang et al. (2011) provided an aluminium electrolytic capacitor example to illustrate the case in which different profiles often have random explanatory variables and these variables require careful monitoring as well. The major objective of this paper is to try to provide a unified framework for Phase II monitoring of generalized linear profiles of which the explanatory variables can be fixed design or random arbitrary design from profile to profile (the monitoring of the explanatory variables is not concerned). In Phase II, we are interested in detecting shifts in the model parameters as quickly as possible, while in Phase I, the purpose is to check the quality of historical data and to obtain accurate estimates of the model parameters.

In this paper, we developed a new control chart for generalized linear profile monitoring, which is based on the weighted likelihood ratio test (WLRT). Our proposed approach can be readily extended to other general profiles or profiles with random predictors if the likelihood function can be obtained. Other likelihood ratio test (LRT) based approaches can be found in Shang et al. (2011), Noorossana et al. (2013b) and Soleymanian et al. (2013). The exponentially weighted moving average (EWMA)-GLM control chart proposed by Shang et al. (2011) made use of all available profile samples up to the current time for estimating parameters, and different profiles are weighted as in an EWMA chart. Nevertheless, we found that the EWMA-GLM control chart has very large short-run false alarms, which renders this chart less useful and unacceptable in practice. Shewhart-type control charts (LRT) were proposed by Noorossana et al. (2013b) and Soleymanian et al. (2013). Another EWMAtype control chart (LRT-EWMA) was proposed by Soleymanian et al. (2013). It is shown that the Shewhart-type LRT control charts perform better at detecting large shifts, while the LRT-EWMA control charts perform better at detecting small to medium shifts. However, compared with our WLRT chart, the LRT-EWMA control chart was not as efficient due to the reason that it only used the current profile samples for estimating parameters, and thus the estimators would have considerably large bias and variance. Numerical results show that our proposed WLRT control chart has satisfactory in-control (IC) run length (RL) distribution and stands out at early detection, where RL is the number of points that must be plotted before a point indicates an out-ofcontrol (OC) condition (Montgomery (2013)).

Now we summarize some abbreviated expressions used in this paper for easy reference.

IC	in-control
OC	out-of-control
RL	run length
ARL	average run length
SDRL	standard deviation of the run length
RMI	relative mean index
CED	conditional expected delay
EWMA	exponentially weighted moving average
MEWMA	multivariate exponentially weighted moving average
GLM	generalized linear models
LRT	likelihood ratio test
WLRT	weighted likelihood ratio test

The remainder of this paper is organized as follows. Our proposed methodology is described in detail in Section 2, including the statistical model and WLRT control chart. Section 3 is devoted to comparing the performance of five methods: WLRT, EWMA-GLM (Shang et al. (2011)), LRT (Noorossana et al. (2013b); Soleymanian et al. (2013)), LRT-EWMA (Soleymanian et al. (2013)) and multivariate EWMA (MEWMA) (Soleymanian et al. (2013)) charts. An illustrative example is given in Section 4. Section 5 concludes this paper and gives further discussion. The algorithm for obtaining the maximum weighted likelihood estimator is summarized in the Appendix.

2 The proposed WLRT scheme

In this section, we closely follow the notation and formulation used in Dobson (2002) to briefly discuss the generalized linear profiles. We assume that the observations are independent within and between profiles.

2.1 The statistical model

At any time point t, for the *i*th profile, our statistical model has three components:

1. Response variables $\tilde{Y}_i = (Y_{i1}, \ldots, Y_{iN})^T$ share the same distribution from the exponential family with a canonical form,

$$f(y_{ij}; \theta_{ij}) = \exp[y_{ij}b(\theta_{ij}) + c(\theta_{ij}) + d(y_{ij})], i = 1, \dots, t, j = 1, \dots, N,$$

where $b(\cdot)$, $c(\cdot)$ and $d(\cdot)$ are known functions and θ_{ij} 's are the parameters of the exponential family of distributions.

2. Explanatory variables

$$\widetilde{X}_{i} = \begin{pmatrix} X_{i1}^{T} \\ \vdots \\ X_{iN}^{T} \end{pmatrix} = \begin{pmatrix} x_{i11} \ \dots \ x_{i1p} \\ \vdots \ \vdots \\ x_{iN1} \ \dots \ x_{iNp} \end{pmatrix},$$

where $X_{ij}^T = (x_{ij1}, \ldots, x_{ijp}), i = 1, \ldots, t, j = 1, \ldots, N$, can be combined linearly with a coefficient vector $\beta = (\beta_1, \ldots, \beta_p)^T$ (where p < N) to form the linear predictor $\eta_{ij} = X_{ij}^T \beta$.

3. A monotone link function $g(\cdot)$ such that

$$g(\mu_{ij}) = \eta_{ij} = X_{ij}^T \beta, i = 1, \dots, t, j = 1, \dots, N,$$

where $\mu_{ij} = E(Y_{ij})$.

Here, the explanatory variables \widetilde{X}_i can be fixed design or random design from profile to profile. We suppose β changes from β_{IC} to another unknown value β_{OC} immediately after an unknown time point τ , which suffices to test the following hypotheses

$$\begin{cases} H_0 : \beta = \beta_{IC}, \\ H_1 : \beta \neq \beta_{IC}, \end{cases}$$

at each time point. Note that β_{IC} can be assumed known for Phase II monitoring.

2.2 Some existing work

From Dobson (2002), we know that, for the ith profile, the log-likelihood function is

$$l_{i}(\beta) = \sum_{j=1}^{N} [y_{ij}b(\theta_{ij}) + c(\theta_{ij}) + d(y_{ij})].$$

To obtain the maximum likelihood estimator of β , we can use the following estimating equation

$$\mathbf{b}_{i}^{(m)} = \mathbf{b}_{i}^{(m-1)} + [\mathbf{\mathfrak{J}}_{i}^{(m-1)}]^{-1} U_{i}^{(m-1)}$$

where $\mathbf{b}_{i}^{(m)}$ is the vector of estimates of β at the *m*th iteration, $[\mathbf{\mathfrak{J}}_{i}^{(m-1)}]^{-1}$ is the inverse of the information matrix, $U_{i}^{(m-1)}$ is the vector of score. When the difference between successive approximations $\mathbf{b}_{i}^{(m-1)}$ and $\mathbf{b}_{i}^{(m)}$ is sufficiently small, $\mathbf{b}_{i}^{(m)}$ is taken as $\hat{\beta}$ (maximum likelihood estimator of β).

Now we briefly review the LRT, LRT-EWMA and MEWMA control charts, which were proposed by Soleymanian et al. (2013) to monitor binary response profiles in Phase II. In fact, the LRT monitoring statistic can be expressed as

$$LRT_i = 2[l_i(\beta_i) - l_i(\beta_{IC})], i = 1, 2, \dots$$

Soleymanian et al. (2013) first normalized the values of LRT_i (here, termed NL_i), and then calculated the statistic of LRT-EWMA control chart by

$$LE_i = \lambda NL_i + (1 - \lambda)LE_{i-1}, i = 1, 2, \dots$$

where λ represents the smoothing parameter and $LE_0 = 0$.

The MEWMA monitoring statistic can be calculated using three steps. We first calculate the following variable

$$Z_i = (\widetilde{X}_i^T W \widetilde{X}_i)^{1/2} (\hat{\beta}_i - \beta_{IC}),$$

where W is an $n \times n$ diagonal matrix (see details in Soleymanian et al. (2013)). Then, we calculate the following statistic

$$E_i = \lambda Z_i + (1 - \lambda) E_{i-1}, i = 1, 2, \dots$$

Finally, the MEWMA monitoring statistic can be calculated by

$$M_i = E_i^T E_i.$$

We will leave the brief review of EWMA-GLM (Shang et al. (2011)) control chart in the next subsection to emphasize the differences of it and our proposed control chart.

2.3 The WLRT control chart

Similar to Qi et al. (2015), up to time point t, the weighted-log-likelihood function can be derived as

$$wl_t(\beta) = \sum_{i=0}^t w_i l_i(\beta) = \sum_{i=0}^t w_i \{ \sum_{j=1}^N [y_{ij}b(\theta_{ij}) + c(\theta_{ij}) + d(y_{ij})] \},$$
(1)

where the weights $w_0 = (1 - \lambda)^t$, $w_i = \lambda(1 - \lambda)^{t-i}$, $i = 1, \dots, t$, and $\lambda \in (0, 1)$ is a smoothing parameter. Here, the observations of $(\widetilde{X}_0, \widetilde{Y}_0)$ can be viewed as pseudo "sample", which are chosen from the IC dataset. We can obtain the $(\widetilde{X}_0, \widetilde{Y}_0)$ from Phase I study or by simulation such that the difference between $\hat{\beta}_0$ (maximum likelihood estimator of β) and β_{IC} is small. In Section 3 and Section 4, we obtain the $(\widetilde{X}_0, \widetilde{Y}_0)$ by simulation, and the random seeds are chosen as 8417 and 123, respectively. Then, we can calculate $l_0(\beta)$ based on $(\widetilde{X}_0, \widetilde{Y}_0)$.

Including the weight w_0 and the observations of Y_0 in Equation (1) has its own merit:

- It ensures that all of the weights sum to one.
- It confirms that the IC run length distribution of our chart proposed below is satisfactory.

Obviously, $wl_t(\beta)$ makes full use of all available samples up to the current time point t, and the more recent samples receive more weight. An analogous idea, which does not include w_0 and the pseudo "sample", has been used by Shang et al. (2011) for binary profile monitoring. Shang et al. (2011) expanded the WLRT statistics to asymptotically equivalent Wald-type charting statistics using standard Taylor's expansion.

Given the value of λ , we can express the WLRT statistic as

$$W_t = 2[wl_t(\beta_t) - wl_t(\beta_{IC})], \qquad (2)$$

where $\hat{\beta}_t = \arg \max_{\beta} w l_t(\beta)$ is the maximum weighted likelihood estimator of β , which can be obtained using the algorithm shown in the Appendix. When the WLRT statistic in Equation (2) is larger than a prespecified upper control limit, we can declare the model parameter β has deviated from the nominal value, which means the process is OC.

Now we summarize the implementation of our proposed WLRT scheme for profile monitoring as follows:

- 1. Obtain the upper control limit for the WLRT control chart by the bisection searching algorithms to achieve the desired IC average run length (ARL). The ARL is the average number of points that must be plotted before a point indicates an OC condition (Montgomery (2013)).
- 2. Begin monitoring the profiles in Phase II. After obtaining the new observations, we calculate the monitoring statistics W_t using Equation (2), and then plot them on the control chart until W_t is larger than the upper control limit.
- 3. After detecting the shift, we identify and remove the root causes, and then monitor the profiles continuously.

It is worth more detailed explanations that, the proposed WLRT control chart used all the profile data upper to the time t (including the IC and OC profile data), but different from the LRT-EWMA control chart, the WLRT chart only estimated one $\hat{\beta}_t$ rather than estimating $\hat{\beta}_1, \ldots, \hat{\beta}_t$ for different profiles. The LRT-EWMA control chart uses the current profile samples for estimating parameters, while the WLRT control chart gives more weight to more recent samples, which ensures that there is no over-reliance on the most recent data. Let k be a sufficiently large integer such that $\lambda(1-\lambda)^k$ close to zero. As t increase, the weights w_1, w_2, \ldots will be close to zero sequentially. In fact, when t is sufficiently large, we only use the most recent k sets of OC profile data to estimate $\hat{\beta}_t$, which ensures that $\hat{\beta}_t$ is close to β_{OC} .

To alleviate the computation burden, when $t \leq k$, we make use of all available samples up to the current time point t to estimate $\hat{\beta}_t$ and calculate W_t . Otherwise, we only use the most recent k sets of sample profile observations, say the observations of $(\widetilde{X}_i, \widetilde{Y}_i), i = t - k + 1, \ldots, t$, to estimate $\hat{\beta}_t$ and calculate W_t . It is worth pointing out that, if $\widetilde{X}_{t-k+1} = \ldots = \widetilde{X}_t$, then $\sum_{i=t-k+1}^t w_i \mathfrak{J}_i = [1 - (1 - \lambda)^k] \mathfrak{J}_t$. Some k values such that $\lambda(1 - \lambda)^k < \varepsilon$ for given ε are given in Table 1. We will choose the small positive value ε as 10^{-7} for simplicity in the next section.

Insert Table 1 about here.

3 Performance comparisons

In this section, we compare the proposed WLRT control chart with four alternative methods, EWMA-GLM (Shang et al. (2011)), LRT (Noorossana et al. (2013b), Soleymanian et al. (2013)), LRT-EWMA (Soleymanian et al. (2013)) and MEWMA (Soleymanian et al. (2013)), to demonstrate the effectiveness of our approach.

Following Amiri et al. (2015) and Shadman et al. (2015), we focus on the Poisson profile in this Section. Similar to Shadman et al. (2015), we assume that the Poisson profiles are as follows:

- a. Response variables Y_{ij} 's are independent Poisson random variables, $j = 1, \ldots, 10$.
- b. Explanatory variables X_{ij} such that
 - when the design points are fixed

$$\left(X_{i1}, X_{i2}, \cdots, X_{i10}\right) = \left(\begin{array}{ccc} x_{i11} & x_{i21} & \cdots & x_{i10,1} \\ x_{i12} & x_{i22} & \cdots & x_{i10,2} \end{array}\right) = \left(\begin{array}{cccc} 1 & 1 & \cdots & 1 \\ 0.1 & 0.2 & \cdots & 1.0 \end{array}\right).$$

- otherwise, for the *i*th profile, nine different design points randomly take values in the above equation.
- c. The log link function such that $g(\mu_{ij}) = \log(\mu_{ij}) = X_{ij}^T \beta$, where $\mu_{ij} = E(Y_{ij})$.

Assume further that the IC parameters β_{IC} is $(1, 1)^T$, while the OC profile parameter at *i*th sample profile is equal to

$$\beta_i = \begin{cases} \beta_{IC}, i = 1, \dots, \tau, \\ \beta_{OC} = \beta_{IC} + \Delta, i = \tau + 1, \dots \end{cases}$$

where $\Delta = (\delta_1 \sigma_1, \delta_2 \sigma_2)^T$, $\delta_1 \neq 0$ or $\delta_2 \neq 0$, and $\sigma_1 = 0.35181$, $\sigma_2 = 0.50947$ are the standard deviation of the maximum likelihood estimator of the profile parameters.

3.1 Comparisons when design points are fixed

For a relatively fair comparison, we adjust the control limits of different charts to make their IC ARL (termed ARL₀) as close as 370 by convention. In comparison of various candidate control charts, ARL is very important and also popular used criterion (Li et al (2014)). When the process is IC, a chart with a larger ARL₀ indicates a lower false alarm rate than other charts. When the process is OC, a chart with a smaller OC ARL (termed ARL₁) indicates a better detection ability of process shifts than other charts. Hereafter, we use the notation h to denote the control limit coefficients, and obtain all results in this section based on 5000 replications. A Fortran program is also available from the authors upon request.

We first study IC performance comparison. Zhou et al. (2012) pointed out

that the IC run length distribution is considered to be satisfactory if it is close to the geometric distribution (Hawkins and Olwell (1998)) or more generally its variation is less than that of a geometric distribution. We use notation Q(.10) and Q(.90) to respectively denote the 10th and 90th percentile of the marginal distribution of the run length. We also study the false-alarm rate for the first 30 observations, $F_{30} = Pr_{IC}(RL \leq 30)$, where $Pr_{IC}(RL \leq 30)$ denotes the probability of run length being less than or equal to 30 when the process is IC. Note that when the run length distribution is geometric, the standard deviation of the run length (SDRL) should be approximately equal to ARL₀, and Q(.10), Median, Q(.90) and F_{30} are about 38, 256, 850 and 0.080 respectively. The IC comparison results are shown in Table 2. Figure 1 presents the cumulative distribution function of IC run-length distributions of the different charts considered when $t \leq 100$.

Insert Table 2 about here.

Insert Figure 1 about here.

Theoretically, the IC run length distribution of a Shewhart-type chart is the geometric distribution. The IC run length distribution of an EWMA-type chart with larger smoothing parameter will be closer to the geometric distribution. It is obvious from Table 2 and Figure 1 that the IC run length distribution of the LRT chart is the most close to the geometric distribution. In addition, the IC performances of the EWMA-GLM, LRT-EWMA, MEWMA and WLRT charts depend on the smoothing parameter, i.e., charts with larger parameters perform better. These findings are consistent with the literature. We can also find that the EWMA-GLM control chart has very large short-run false alarms. For example, F_{30} can be as large as 0.183 when $\lambda = 0.2$, and 0.355 when $\lambda = 0.05$. Consequently, the EWMA-GLM control chart is not acceptable in terms of run length distribution because excessive false alarms at early runs will make the detection results unreliable. Moreover, the probabilities of very long runs would decrease, which will lead to the EWMA-GLM control chart having quite small ARL₁ compared to the LRT, LRT-EWMA, MEWMA and WLRT charts. However, this "advantage" is mainly due to very large shortrun false alarms, which is consistent with Zhou et al. (2012). Following Zhou et al. (2012), we will also consider the "true" detection capability as another criterion for the OC performance comparison.

Then, we study the OC performance comparison. For the zero state (shift occurs at $\tau = 0$), we compare the ARL₁, the "true" detection capability and the relative mean index (RMI). The "true" detection capability of a chart is reflected by the quantity γ_t , where

$$\gamma_t = Pr_{OC}(RL \le t) - Pr_{IC}(RL \le t).$$

Here, γ_t is a reasonable index for OC comparison given that the RL distribu-

tions of some charts are far away from geometric, and a control chart with a larger value of γ_t is considered better (Zhou et al. (2012)). In order to assess the overall performance of different charts, we compare the RMI values. The RMI index of a control chart, suggested by Han and Tsung (2006), is defined as

$$RMI = \frac{1}{M} \sum_{l=1}^{M} \frac{ARL_{\Delta l} - MARL_{\Delta l}}{MARL_{\Delta l}},$$

where M is the total number of shifts considered, $\operatorname{ARL}_{\Delta l}$ is the ARL_1 of the given control chart when detecting a parameter shift of magnitude Δl , and $\operatorname{MARL}_{\Delta l}$ is the smallest among all ARL_1 values of the charts considered when detecting the shift Δl . A control chart with a smaller RMI value is considered better in its overall performance (Zhou et al. (2012)). As for the steady state, we compare the conditional expected delay (CED) (Kenett and Zacks (1998); Lee et al. (2012)) as the detection ability depends on the time point of the change (Sonesson and Bock (2003)). The CED is defined by

$$CED = E[RL - \tau | RL > \tau].$$

A control chart with a smaller CED value is considered better than another one. The comparisons of ARL_1 and RMI values are reported in Table 3.

Insert Table 3 about here.

From Table 3, we can see that the EWMA-GLM ($\lambda = 0.05$) chart outperforms other competitors considering the overall performance. Additionally, the LRT control chart performs better at detecting large shifts, while the LRT-EWMA, MEWMA and WLRT control charts perform better at detecting small to medium shifts. We can also find that the performance of the LRT-EWMA, MEWMA and WLRT control charts depend on the smoothing parameter, i.e., charts with smaller parameter λ perform better for detecting small shifts, while those with larger parameter λ perform better for detecting larger shifts. Figure 2 presents the "true" detection capability γ_t of the different charts considered when $t \leq 100$. We can see that, when t is small, the EWMA-GLM chart outperforms the other four charts in the sense that its γ_t curve increases much faster. But this advantage diminishes quickly as t becomes large due to its very large false alarms. In general, the WLRT chart performs better than the MEWMA chart, and the MEWMA chart performs better than the LRT-EWMA and LRT charts. We can also find that, the LRT chart performs worst at detecting small and medium shifts.

Insert Figure 2 about here.

Recall that we recommend to use the most recent k sets of profile observations when t > k. Table 4 shows that, when the integer k is sufficiently large, it has little effect on the performance of the WLRT chart. Table 5 provides the comparison results of CEDs. We discard any series in which a signal occurs before the $(\tau + 1)$ th observation. This action coincides with the proposals presented by Zhou et al. (2012) and Hawkins and Olwell (1998). We only present the CED's results when $\tau = 50$ for illustration purpose, and a similar conclusion holds for other cases. It is clear that the performance of the WLRT chart is satisfactory, especially when the shifts are small.

Insert Table 4 about here.

Insert Table 5 about here.

3.2 Comparisons when design points are not fixed

In this subsection, we consider the case in which the explanatory variables are not fixed from profile to profile. Note we will, here, not focus on the monitoring of the explanatory variables themselves. If it is concerned instead, we need change the weighted-log-likelihood function in Equation (1) correspondingly. To generate the values of the explanatory variables, we first generate an integer j from a discrete uniform distribution over the integers from 1 to 10. Then, we delete the corresponding jth design point X_{ij} from the ten design points $X_{i1}, X_{i2}, \dots, X_{i10}$. In this way, we get nine different design points. By similar ways, we get other number of different design points. Here, we use the same control limits as those in Table 2. We only present the OC comparison results when $\tau = 0$ and $\tau = 50$ in Table 6 and Table 7 respectively for illustration purpose. We find that the performance of the WLRT chart with parameter $\lambda = 0.05$ is still satisfactory, especially when the shifts are small.

Insert Table 6 about here.

Insert Table 7 about here.

Finally, we consider the effects of the number and values of design points on our WLRT control chart. The ARL performances of WLRT chart depending on different number of design points are given in Table 8. The first 50 design points used in Table 8 based on 1 simulation run are shown in Figure 3. From Table 8, the performance is better when the number of design points is larger.

Insert Table 8 about here.

Insert Figure 3 about here.

4 Illustrative example

In this section, we adopt and extend the multinomial logistic regression model discussed by Goeman and Cessie (2006) as an illustrative example. In the production processes, no product is created quite the same as the others due to the machine equipment, material, environment, operator, and some other reasons (Chen et al. (2011)). Instead of simply classifying qualities into conforming and non-conforming, products can be classified into several classes of quality. Details of the multinomial logistic regression are referred to Dobson (2002) and Hosmer et al. (2013), and please refer Böhning (1992) and Hasan et al. (2014) as for its algorithm.

Multinomial logistic regression is often used when the response variable is categorical, with more than two categories. Two variants exist: one for nominal and one for ordinal scale outcomes. Here, we consider only the nominal scale version. For ease of exposition, we will suppress the index "i" and "j" which were used in Section 2. Consider a response variable Y with four categories. Let π_1, \ldots, π_4 denote the respective probabilities, with $\pi_1 + \ldots + \pi_4 = 1$. We consider a case with three covariates as follows

$$\log(\frac{\pi_2}{\pi_1}) = 2x_1 + \delta x_1^2$$
$$\log(\frac{\pi_3}{\pi_1}) = 2x_2,$$
$$\log(\frac{\pi_4}{\pi_1}) = 2x_3,$$

where x_1 , x_2 and x_3 each takes values -1, 0 and 1. At each time point t, we obtained a data set of 25 observations which were taken randomly from each of the $3^3 = 27$ possible combinations of the three covariate values.

Here, we extend the Newton-Raphson method in Hasan et al. (2014) to estimate the model parameters, and adjust the control limits of different charts to make their ARL₀ as close as 370 based on 5000 replicates. The first 20 profiles are generated from the IC ($\delta = 1$) normal operational condition and the remaining profiles are from the OC ($\delta = 1.6$) condition. The smoothing parameter λ is chosen as 0.1 for the LRT-EWMA and WLRT control charts. The LRT, LRT-EWMA and WLRT control charts are constructed in Figure 4. From Figure 4, we can see that the performance of the WLRT chart is satisfactory.

Insert Figure 4 about here.

5 Conclusion remarks

In this paper, we proposed a unified framework for Phase II monitoring of generalized linear profiles. In practical applications, it is not uncommon to encounter quality characteristics that are either count data or categorical in nature. Such quality characteristics are often modeled as special cases of generalized linear models. Thus, statistical process control monitoring is important and challenging for generalized linear profiles. The proposed control chart is essentially based on calculating the weighted log-likelihood ratio test statistics, which can be readily extended to other general profiles or profiles with random predictors if the likelihood function can be obtained. Numerical results show that the proposed control chart has satisfactory in-control run length distribution and stands out at early detection.

Our proposed scheme assumes that the observations are independent within and between profiles. The cases when observations are dependent, warrant further investigation.

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Appendix

In this Appendix, we briefly introduce how to estimate $\hat{\beta}_t$, which is the maximum weighted likelihood estimator of β . Let $\mathfrak{J} = \sum_{i=0}^t w_i \mathfrak{J}_i$ and $U = \sum_{i=0}^t w_i U_i$. According to Dobson (2002), we can see, if $\widetilde{X}_0 = \ldots = \widetilde{X}_t$, then $\mathfrak{J}_0 = \ldots = \mathfrak{J}_t$, and then $\mathfrak{J} = \mathfrak{J}_1$. The proposed Newton-Raphson approximation for obtaining $\hat{\beta}_t$ proceeds as follows:

- (1) Start with the initial values of β , denoted as $\beta^{(0)}$.
- (2) Calculate $\mathfrak{J}^{(m)}$ and $U^{(m)}$, by using $\beta^{(m)}$ in the *m*th iteration.
- (3) Update the estimation of β as follows:

$$\beta^{(m+1)} = \beta^{(m)} + [\mathfrak{J}^{(m)}]^{-1} U^{(m)}$$

(4) Repeat steps (2) and (3) until adequate convergence is achieved as follows:

$$\| \beta^{(m)} - \beta^{(m-1)} \|_1 / \| \beta^{(m-1)} \|_1 \le \epsilon,$$

where ϵ is a given small positive value (e.g., $\epsilon = 10^{-4}$) and $\|\beta\|_1$ denotes L_1 norm, that is, the sum of the absolute values of all elements of β . As such, $\hat{\beta}_t = \beta^{(m)}$ is the desired estimator of β .

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Fig. 1. The in-control cumulative distribution function curves for the Poisson profiles along with Geometric distribution (with expectation 370).

Table	1
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k value	k values such that $\lambda(1-\lambda)^k < \varepsilon$										
	ε										
λ	10^{-4}	10^{-5}	10^{-6}	10^{-7}	10^{-8}	10^{-9}	10^{-10}				
0.05	122	167	211	256	301	346	391				
0.1	66	88	110	132	153	175	197				
0.2	35	45	55	66	76	86	96				



Fig. 2. The "true" detection capability for the Poisson profiles ($\lambda = 0.05$). The legend in the last plot is applicable for all the others.



6 different design points

Fig. 3. The first 50 design points used in Table 8 based on 1 simulation run.

7 different design points



Fig. 4. The LRT, LRT-EWMA and WLRT control charts for the multinomial profiles.

Table 2 IC comparisons

	h	ARL_0	SDRL	Q(.10)	Median	Q(.90)	F_{30}
EWMA-GLM0.05	9.90756	370	520	2	154	1040	0.355
EWMA-GLM0.2	11.60040	370	409	4	239	922	0.183
LRT	11.89143	370	369	38	258	850	0.083
LRT-EWMA0.05	0.68820	370	348	63	261	813	0.022
LRT-EWMA0.2	1.47790	370	370	43	256	850	0.069
MEWMA0.05	0.31650	370	338	57	268	826	0.030
MEWMA0.2	1.55000	370	353	43	265	839	0.068
WLRT0.05	0.22710	370	369	47	255	853	0.055
WLRT0.2	1.22170	370	371	40	257	845	0.075

Table 3

Comparisons of ARL₁ for the Poisson profiles $(\tau = 0)$

	LRT	EWMA-	GLM	LRT-E	WMA	MEW	VMA	WL	RT
(δ_1,δ_2)		$\lambda = 0.05$	0.2	0.05	0.2	0.05	0.2	0.05	0.2
(0.2,0)	201(199)	18.9(19.8)6	7.2(71.3)	125(102)	153(151)	95.5(72.3)	365(366)	26.4(17.4)	44.8(39.6)
(0,0.2)	202(209)	18.3(19.3)6	4.3(67.8)	124(100)	154(152)	79.2(55.7)	265(255)	26.1(17.3)	45.1(39.5)
(0, 0.25)	151(152)	11.8(11.5)3	5.0(35.8)	81.9(61.7)	102(99.7)	45.5(25.9)	130(123)	18.4(10.6)	27.5(22.4)
(0.31,0)	106(107)	8.31(7.22)2	0.0(19.4)	52.4(35.2)	62.9(58.5)	31.6(15.7)	70.8(61.6)	13.5(6.82)	17.5(13.2)
(0.2, 0.2)	64.0(65.7)	5.55(4.28)1	0.5(9.21)	31.5(18.2)	33.2(29.3)	20.1(7.71)	28.7(21.2)	9.74(4.19)	10.8(7.05)
$(0.5,\!0)$	33.9(33.8)	3.77(2.62)5	.90(4.49)	18.4(8.87)	16.3(12.5)	13.9(4.20)	14.1(8.24)	7.10(2.63)	6.89(3.65)
(0.32,0.32))16.1(15.4)	2.65(1.62)3	.62(2.44)	11.3(4.87)	8.47(5.55)	10.1(2.50)	8.29(3.63)	5.34(1.73)	4.76(2.15)
(0,0.7)	10.6(10.2)	2.20(1.27)2	.90(1.77)	8.76(3.56)	6.24(3.73)	8.67(1.89)	6.58(2.49)	4.63(1.38)	3.98(1.63)
(0.44,0.44)	5.30(4.72)	1.69(0.86)2	.06(1.11)	5.78(2.22)	3.89(2.08)	6.84(1.30)	4.77(1.45)	3.65(0.99)	3.02(1.07)
(0.59, 0.59)	2.03(1.45)	1.21(0.44)1	.35(0.57)	3.23(1.13)	2.10(0.97)	4.96(0.76)	3.21(0.74)	2.61(0.64)	2.09(0.62)
(1.0, 1.0)	1.01(0.08)	1.00(0.02)1	.00(0.03)	1.22(0.41)	1.02(0.15)	3.00(0.21)	1.99(0.16)	1.49(0.50)	1.07(0.26)
RMI	6.679	0.00	0.993	3.795	3.920	2.932	5.882	0.779	0.930

 1 NOTE: Standard deviations are in parentheses.

		$\lambda = 0.05$			$\lambda = 0.2$	
(δ_1,δ_2)	k = 122	256	391	35	66	96
$(0,\!0)$	368.68(366.19)	369.86(368.53)	369.86(368.53)	369.05(370.83)	369.82(371.28)	369.82(371.28)
(0.2,0)	26.354(17.418)	26.354(17.418)	26.354(17.421)	44.795(39.551)	44.795(39.551)	44.788(39.546)
(0,0.2)	26.060(17.260)	26.060(17.260)	26.060(17.260)	45.047(39.441)	45.064(39.475)	45.064(39.475)
(0, 0.25)	18.362(10.631)	18.362(10.631)	18.362(10.631)	27.450(22.351)	27.455(22.368)	27.455(22.368)
(0.31,0)	13.481(6.815)	13.481(6.815)	13.481(6.814)	17.489(13.197)	17.489(13.197)	17.489(13.197)
(0.2, 0.2)	9.735(4.192)	9.735(4.192)	9.735(4.191)	10.842(7.047)	10.842(7.047)	10.842(7.047)
(0.5,0)	7.098(2.630)	7.098(2.630)	7.098(2.630)	6.887(3.648)	6.887(3.648)	6.889(3.648)
(0.32, 0.32)	5.339(1.725)	5.339(1.725)	5.339(1.725)	4.761(2.148)	4.761(2.148)	4.761(2.148)
$(0,\!0.7)$	4.632(1.381)	4.632(1.381)	4.632(1.381)	3.982(1.628)	3.982(1.628)	3.981(1.628)
(0.44, 0.44)	3.647(0.993)	3.647(0.993)	3.647(0.993)	3.020(1.069)	3.020(1.069)	3.020(1.069)
(0.59, 0.59)	2.614(0.642)	2.614(0.642)	2.614(0.642)	2.091(0.620)	2.091(0.620)	2.091(0.620)
(1.0, 1.0)	1.489(0.500)	1.489(0.500)	1.489(0.500)	1.071(0.257)	1.071(0.257)	1.071(0.257)

Table 4 The ARL of WLRT chart with different $k~(\tau=0)$

 1 NOTE: h is same as Table 2, standard deviations are in parentheses.

Table 5	
Comparisons of CEDs for the Poisson profiles ($\tau = 50$)	

	LRT	EWMA	A-GLM	LRT-E	EWMA	MEV	VMA	WI	LRT
(δ_1,δ_2)		$\lambda = 0.05$	0.2	0.05	0.2	0.05	0.2	0.05	0.2
(0.2,0)	201(200)	35.4(23.3)	77.4(72.1)	107(100)	151(151)	98.7(72.9)	364(367)	29.7(19.4)	44.8(40.4)
(0,0.2)	201(208)	35.0(23.3)	74.3(67.5)	107(98.9)	151(151)	80.1(57.8)	261(253)	29.3(19.1)	44.3(40.5)
(0, 0.25)	152(152)	24.3(14.0)	42.1(37.2)	68.8(61.4)	98.6(99.3)	47.7(27.6)	127(120)	21.0(11.7)	27.7(22.8)
$(0.31,\!0)$	106(108)	17.7(8.92)	25.2(20.2)	43.0(36.4)	60.4(57.8)	33.9(16.4)	69.6(61.8)	15.9(8.14)	17.9(13.7)
(0.2, 0.2)	64.2(65.1)	12.7(5.69)	14.3(9.78)	24.2(17.8)	31.5(29.1)	21.9(8.48)	28.4(21.5)	11.5(5.37)	11.2(7.46)
$(0.5,\!0)$	34.1(34.5)	9.25(3.87)	8.72(4.82)	13.5(8.79)	15.1(12.5)	15.5(4.98)	14.4(8.59)	8.50(3.65)	7.23(3.94)
(0.32,0.32))16.5(16.2)	6.93(2.68)	5.71(2.66)	8.07(4.71)	7.86(5.76)	11.2(3.34)	8.58(3.81)	6.47(2.57)	4.99(2.32)
(0,0.7)	10.8(10.5)	5.94(2.23)	4.71(2.02)	6.20(3.53)	5.67(3.85)	9.49(2.69)	6.76(2.69)	5.55(2.16)	4.15(1.85)
(0.44,0.44)) 5.28(4.68)	4.71(1.66)	3.53(1.37)	4.07(2.12)	3.42(2.03)	7.66(1.99)	4.97(1.65)	4.42(1.64)	3.13(1.24)
(0.59, 0.59)) 2.03(1.45)	3.36(1.13)	2.39(0.79)	2.30(1.06)	1.89(0.92)	5.55(1.34)	3.33(0.91)	3.15(1.10)	2.18(0.75)
(1.0, 1.0)	1.01(0.08)	1.86(0.57)	1.28(0.45)	1.06(0.24)	1.01(0.12)	3.31(0.75)	1.94(0.45)	1.76(0.57)	1.19(0.39)
RMI	3.332	0.365	0.559	1.176	1.697	1.523	3.067	0.242	0.163

 1 NOTE: Standard deviations are in parentheses.

Table 6						
Comparisons of ARL_1	when the	design	points a	are not	fixed $(\tau = 0$)

	LRT	EWMA	A-GLM	LRT-E	WMA	MEV	VMA	WI	LRT
(δ_1,δ_2)		$\lambda = 0.05$	0.2	0.05	0.2	0.05	0.2	0.05	0.2
(0,0)	368(371)	364(520)	367(415)	363(333)	368(370)	335(301)	319(308)	377(368)	369(371)
(0.2,0)	213(216)	21.0(22.4)	78.2(84.4)	134(110)	164(159)	116(91.5)	460(458)	29.5(19.7)	51.0(45.2)
(0, 0.2)	208(212)	20.3(22.1)	74.7(79.3)	133(110)	162(157)	95.1(72.5)	312(305)	29.2(19.3)	49.8(44.5)
(0, 0.25)	157(158)	13.2(13.1)	40.9(42.6)	90.0(69.1)	111(106)	53.0(32.3)	161(157)	20.6(11.9)	31.2(25.8)
(0.31,0)	114(113)	9.11(8.16)	23.0(22.3)	58.4(40.6)	70.8(66.3)	35.8(18.7)	91.0(83.1)	15.0(7.67)	19.9(15.3)
(0.2, 0.2)	71.0(70.9)	6.11(4.78)	12.0(10.8)	34.7(20.3)	38.2(33.7)	22.2(8.81)	34.8(27.0)	10.8(4.69)	12.1(8.06)
$(0.5,\!0)$	38.6(38.4)	4.13(2.95)	6.67(5.19)	20.5(10.4)	18.8(14.7)	15.1(4.82)	16.4(10.3)	7.87(2.98)	7.77(4.20)
(0.32, 0.32)	18.7(18.2)	2.86(1.80)	4.06(2.82)	12.4(5.56)	9.75(6.65)	10.9(2.85)	9.24(4.39)	5.88(1.93)	5.32(2.45)
(0,0.7)	12.2(12.0)	2.39(1.41)	3.21(2.05)	9.62(3.99)	7.06(4.44)	9.32(2.13)	7.27(2.90)	5.13(1.58)	4.43(1.88)
(0.44,0.44)	6.09(5.42)	1.82(0.95)	2.26(1.25)	6.40(2.51)	4.34(2.42)	7.30(1.43)	5.21(1.67)	4.02(1.12)	3.32(1.20)
(0.59, 0.59)	2.31(1.73)	1.27(0.51)	1.45(0.64)	3.52(1.27)	2.31(1.10)	5.26(0.83)	3.45(0.84)	2.87(0.71)	2.28(0.69)
(1.0, 1.0)	1.01(0.12)	1.00(0.04)	1.00(0.05)	1.31(0.47)	1.04(0.20)	3.09(0.30)	2.02(0.16)	1.66(0.48)	1.16(0.37)
RMI	6.598	0.00	1.068	3.797	3.944	3.036	6.545	0.823	0.980

 1 NOTE: h is same as Table 2, standard deviations are in parentheses.

	LRT	EWMA	A-GLM	LRT-E	WMA	MEW	VMA	WL	RT
(δ_1,δ_2)		$\lambda = 0.05$	0.2	0.05	0.2	0.05	0.2	0.05	0.2
(0.2,0)	212(213)	38.5(25.8)	88.9(85.1)	115(108)	162(158)	120(93.1)	459(461)	32.3(21.2)	50.8(45.8)
(0,0.2)	209(208)	38.4(25.6)	84.7(79.6)	115(109)	158(155)	94.6(71.2)	305(301)	31.9(20.9)	49.8(45.7)
(0, 0.25)	159(161)	26.5(15.8)	48.8(43.6)	75.1(67.6)	108(106)	55.2(34.1)	161(158)	23.0(13.4)	31.2(26.0)
$(0.31,\!0)$	113(113)	19.2(9.96)	28.9(23.2)	48.1(40.6)	67.8(65.5)	39.1(19.8)	89.1(82.6)	17.0(8.97)	19.8(15.5)
(0.2, 0.2)	70.2(70.0)	13.7(6.29)	16.2(11.6)	26.8(19.9)	36.2(33.2)	24.4(10.0)	35.0(27.7)	12.3(5.90)	12.3(8.38)
(0.5,0)	38.3(39.3)	9.90(4.14)	9.58(5.68)	15.2(10.3)	17.5(15.0)	17.0(5.79)	17.1(10.6)	9.00(3.90)	7.79(4.53)
(0.32, 0.32))18.9(18.6)	7.39(2.89)	6.26(3.08)	8.89(5.27)	8.93(6.67)	12.2(3.72)	9.55(4.61)	6.90(2.78)	5.34(2.60)
(0,0.7)	12.3(12.4)	6.35(2.39)	5.14(2.33)	6.83(3.91)	6.40(4.51)	10.2(2.95)	7.49(3.17)	5.88(2.32)	4.47(2.02)
(0.44,0.44)) 6.03(5.42)	4.99(1.79)	3.80(1.51)	4.47(2.34)	3.89(2.42)	8.23(2.15)	5.34(1.87)	4.70(1.73)	3.32(1.34)
(0.59, 0.59))2.30(1.74)	3.56(1.17)	2.53(0.88)	2.49(1.18)	2.06(1.03)	5.93(1.43)	3.59(1.00)	3.31(1.16)	2.29(0.84)
(1.0, 1.0)	1.02(0.12)	1.93(0.61)	1.36(0.49)	1.11(0.31)	1.03(0.17)	3.49(0.79)	2.04(0.47)	1.85(0.59)	1.27(0.44)
RMI	3.320	0.363	0.619	1.202	1.739	1.627	3.534	0.236	0.183

Table 7 Comparisons of CEDs when the design points are not fixed ($\tau = 50$)

 1 NOTE: h is same as Table 2, standard deviations are in parentheses.

	the number of design points										
(δ_1,δ_2)	10	9	8	7	6						
(0,0)	370(369)	377(368)	373(358)	367(351)	383(348)						
$(0.2,\!0)$	26.4(17.4)	29.5(19.7)	33.1(22.5)	38.6(25.9)	45.6(30.4)						
(0,0.2)	26.1(17.3)	29.2(19.3)	33.2(22.5)	38.7(26.4)	46.0(30.8)						
(0, 0.25)	18.4(10.6)	20.6(11.9)	23.4(14.1)	27.3(16.1)	32.4(19.7)						
$(0.31,\!0)$	13.5(6.82)	15.0(7.67)	17.0(8.90)	19.6(10.0)	23.3(12.4)						
(0.2, 0.2)	9.74(4.19)	10.8(4.69)	12.2(5.44)	14.0(6.26)	16.5(7.59)						
$(0.5,\!0)$	7.10(2.03)	7.87(2.98)	8.84(3.39)	10.0(3.83)	11.8(4.67)						
(0.32, 0.32)	5.34(1.73)	5.88(1.93)	6.60(2.24)	7.52(2.54)	8.76(3.06)						
(0,0.7)	4.63(1.38)	5.13(1.58)	5.70(1.82)	6.49(2.11)	7.57(2.53)						
(0.44, 0.44)	3.65(0.99)	4.02(1.12)	4.47(1.27)	5.05(1.46)	5.86(1.70)						
(0.59, 0.59)	2.61(0.64)	2.87(0.71)	3.17(0.80)	3.55(0.90)	4.11(1.04)						
(1.0, 1.0)	1.49(0.50)	1.66(0.48)	1.82(0.43)	1.98(0.43)	2.20(0.51)						

Table 8 The ARL of WLRT chart with different number of design points

 1 NOTE: $\lambda=0.05, \tau=0, h$ is same as Table 2, standard deviations are in parentheses.